



Scan to know paper details and
author's profile

Determination of Manufacturing Parameters for Maintaining form Accuracy of Packaging Support Block Made with Polyurethane Foam

Jiwan Kang, Heeyoung Maeng & Suin Eun

ABSTRACT

A support block for packaging valuables usually uses a material with surface elasticity, such as polyurethane foam or polystyrene foam. This is to ensure that the surface can be well contacted and supported so that the contents of the package can be protected from vibration or shock when valuables are transported over long distances. In general, this polyurethane packaging support block is manufactured using an NC milling machine and a ball nosed end mill tool specially designed to cut the cushioned soft materials. However, because the elastic cushion of the material is very large, it is very difficult to implement the 3D form accuracy that can be in good contact with the surface of the packaged contents. This study tried to explore the manufacturing parameters that could maintain the good contact with the surface form of packaged valuables accurately and could support the contents stably, through the Taguchi technique, that minimizes the influence of uncontrollable factors through controllable factors.

Keywords: packaging support block; nc milling of polyurethane foam; manufacturing parameters; taguchi technique; form accuracy; vibration test.

Classification: DDC Code: 668.4,LCC Code: TP1122

Language: English



LJP Copyright ID: 392923

Print ISSN: 2631-8474

Online ISSN: 2631-8482

London Journal of Engineering Research

Volume 22 | Issue 2 | Compilation 1.0



© 2022. Jiwan Kang, Heeyoung Maeng & Suin Eun. This is a research/review paper, distributed under the terms of the Creative Commons Attribution- Noncom-mercial 4.0 Unported License (<http://creativecommons.org/licenses/by-nc/4.0/>), permitting all noncommercial use, distribution, and reproduction in any medium, provided the original work is properly cited.

Determination of Manufacturing Parameters for Maintaining form Accuracy of Packaging Support Block Made with Polyurethane Foam

Jiwan Kang^a, Heeyoung Maeng^a & Suin Eun^b

ABSTRACT

A support block for packaging valuables usually uses a material with surface elasticity, such as polyurethane foam or polystyrene foam. This is to ensure that the surface can be well contacted and supported so that the contents of the package can be protected from vibration or shock when valuables are transported over long distances. In general, this polyurethane packaging support block is manufactured using an NC milling machine and a ball nosed end mill tool specially designed to cut the cushioned soft materials. However, because the elastic cushion of the material is very large, it is very difficult to implement the 3D form accuracy that can be in good contact with the surface of the packaged contents. This study tried to explore the manufacturing parameters that could maintain the good contact with the surface form of packaged valuables accurately and could support the contents stably, through the Taguchi technique, that minimizes the influence of uncontrollable factors through controllable factors. Using the characteristics value by Taguchi technique based on the experimental accumulated machining data under similar environment, the optimal manufacturing parameters such as the spindle speed, feedrate, step over, and tool path pattern were determined. And the manufacturing parameters determined through these analysis techniques have been verified practically by testing experiment using a group of expert's machining data. Also, in order to examine the suitability of these parameters, the prediction accuracy was confirmed by comparing it with a large amount of experimental data accumulated by experts. In addition, in order to confirm the packaging performance of the support block manufactured under these parameters, the vibration test were

performed on these samples to compare and analyze whether they satisfied the limits of the standard specification.

Keywords: packaging support block; nc milling of polyurethane foam; manufacturing parameters; taguchi technique; form accuracy; vibration test.

I. INTRODUCTION

With the recent development of the logistics industry and the exhibition fair event, it is increasingly necessary to safely transport valuables such as electronic products, expensive artworks, sculptures, jewelry, antiques, and cultural assets to long distances. When these valuables are safely transported, they usually go through a special packaging process, and most of them rely on the experience of experts. Companies specializing in this packaging industry use the cushioned and soft standardized packaging support block made of polyurethane or polystyrene block to effectively wrap the contents goods.

The support block used for this purpose should have adequate elasticity and protects the valuables from external impact as it is in contact with the content goods. To do this, the shape of the curved surface must have the consistent clearance so that the inner contact surface of the support block can smoothly contact the outer surface of the content goods [1]. The curved surface of support block is made into a suitable form by giving a uniformed margin considering the gap and pressing tolerance based on the contact region of the outer surface of the valuables, and then it is designed so that the surface of soft material foam is to be machined easy using NC (Numerical control) milling machine while satisfying the machining allowance [2].

At this time, deformation occurs in areas subject to excessive pressure due to poor form accuracy. If there is a gap with insufficient contact, external vibration cannot be blocked and damage such as scratches or cracks may occur on the content surfaces. When it is machined at NC milling machine, unlike when machining metal or hard materials, it uses a specialized ball nosed end mill tool having a needle protrusion on the cutter blade. Therefore, cushioned deformation on the surface of support block is inevitable.

Regarding this special machining cases, Kim et al. [3], as part of an effort to increase the surface roughness of the workpiece when NC milling of relatively light epoxy foam, the cutting conditions such as appropriate spindle rotation speed, axial depth of cut, are experimentally determined. Also, Min [4] and Zhang [5] calculated the amount of tool offset by considering the deformation of the contact surface between a specially manufactured tool and a workpiece when NC milling a soft polyurethane foam material.

In addition, Shim et al. [6] have studied a method for estimating the shock absorption rate of polyurethane foam through the speed at which the steel balls were dropped. Furthermore, Kim et al. [7] have suggested the dropping simulation of the outdoor unit of an air conditioner in a state of being packaged with polyurethane foam, and through these simulation data, they found the weakened regions and reinforced areas of the packaging support block.

However, there have been no research so far in which the manufacturing parameters have been decided to maintain form accuracy when machining the polyurethane foams, and no research has been conducted on the effect of interference and clearance gaps of the support block.

This study investigated the method of determining the manufacturing parameters that can maintain the form accuracy of the contact surface so that the support block can stably support the content goods. A new method using Taguchi technique [8, 9] are proposed to find the optimal manufacturing parameters, which is not

only feed speed and spindle speed, but also many factors such as machining direction, axial depth of cutting, and spacing between paths, act in a complex manner. And this method evaluated its applicability on the empirical data from a group of experts accumulated for a long time, and through a vibration test on the packaging support block in which manufacturing parameters were applied to the actual packaging process.

II. MANUFACTURING PROCEDURE OF PACKAGING SUPPORT BLOCK

The manufacturing process of packaging support block goes through the process as shown in Figure 1 generally. A 3D scanner is used to collect 3D scan data for the surface of the packaged object, and the shape of the support block form is designed based on the collected 3D data. At this time, after correcting the curved surface in consideration of gaps, elastic margins, and gouging, the tool path data for NC milling is generated for the curved surface of the contact part with the content goods.

Then, this NC data is input into the NC milling machine, and the milling work is performed on the table to complete the machining of the support block form. The next step is to assemble the various sub-elements that make up the packaging support block, and then place the contents inside the support block for packaging. This polyurethane foam has elasticity, but has stability in temperature change, chemical stability, shock and external vibration. Table 1 shows a comparison of three representative physical properties(i.e., conductivity, elastic modulus, and pH) for the two materials of foam, such as polyurethane material and EVA (ethylen-vinyl acetate) foam.

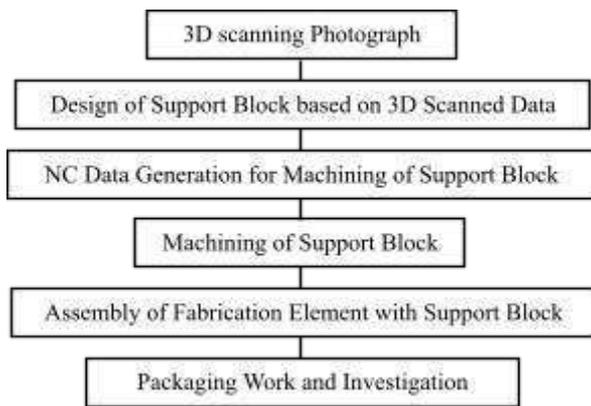


Figure 1: Process chart for manufacturing of packaging support block

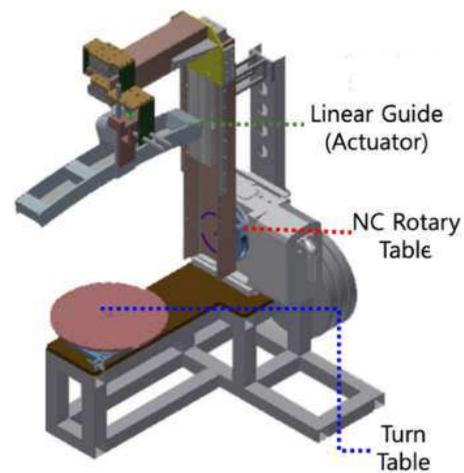


Table 1: Properties of packaging support block materials

Materials	Polyurethane foam	Eva foam
Conductivity ($W \cdot m^{-1} \cdot K^{-1}$)	0.024	0.038
Elastic Modulus (MPa)	0.34	0.49
pH	6.7	6.3

2.1 Collection of shape data using 3D scanning

Although there are various scanning methods depending on the complexity of the shape to scan the surface of the package content goods, a spherical coordinate system 3D scanner is widely used as equipment for easy automatic scanning on a desktop. This is because it is good to measure all surfaces at once in one place without moving valuables as much as possible by adjusting the longitude and latitude angles of the spherical coordinate system.

Figure 2 shows a typical spherical coordinate system 3D scanner. When data are collected using this spherical coordinate system, automatic scanning is performed using a macro after performing zero adjustment and calibration using a standard master ball. There is almost no loss time except for the time gap between scanner shooting and instrument setting, so high-speed scanning with high resolution is possible. After the scanning work is completed, the acquired data is automatically converted into the world coordinate system through the commercial application software.

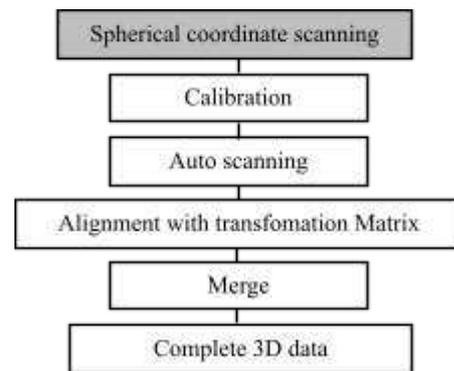


Figure 2: Spherical coordinate system device and 3D scanning process

2.2 Design of support block based on 3D scanned data

Figure 3 shows the scanned sample of a sculptured surface for content goods on a support block based on the scanned 3D data. At this time, the work of correcting the sculptured surface is performed in consideration of gaps, tolerances, and margins.

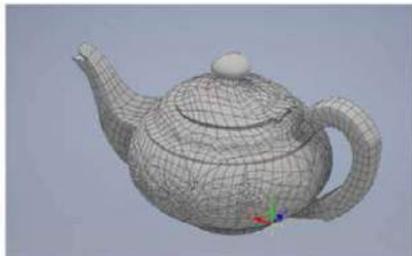


Figure 3: Scanned 3D data sample of packaging content goods

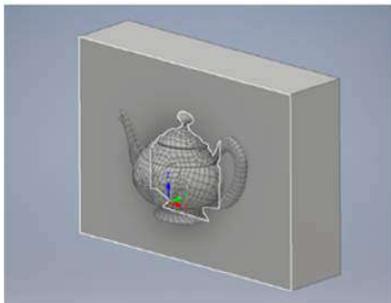
As the first step, as shown in Figure 4(a), the scan data of the packaged content goods is merged and placed at the world coordinate origin, and the size of the packaging support block is laid out in a rectangular shape as shown in Figure 4(b).

And then, as shown in Figure 4(c), after placing them in a symmetrical structure at the center, it performed offsetting work considering gaps, tolerances, and margins to the normal direction of the curved surface. Finally, the cavity sculpture surface of the lower support block is completed by removing the protruded surface beyond the block boundary as shown in Figure 4(d).

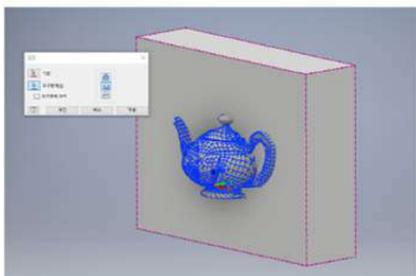
Also, the design process of upper support block is applied as the same design steps of lower support block. Then the whole design process is completed.



(a) Original scanned model



(b) Sizing of support frame block



(c) Offsetting margin and clearance

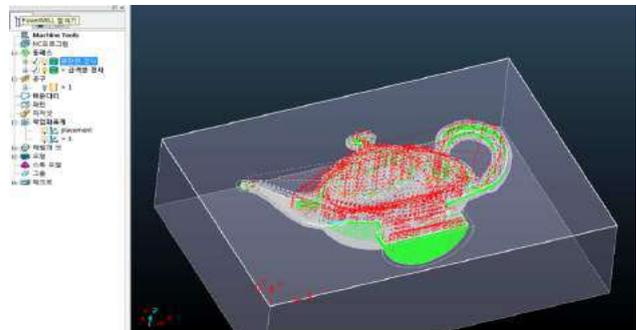


(d) Completed lower support block

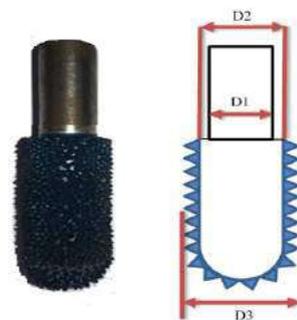
Figure 4: Design process of support block based on 3D scan data

2.3 Cutting path generation for sculpture surface

The inner sculptured surface of support block goes through the process of calculating the cutting path for NC milling as shown in Figure 5(a), and the cutting tool used here is a special tool in the form of a ball end mill on which has a needle-shaped protrusion as shown in Figure 5(b). This cutting path uses a lot of contour line cutting paths so that the slope condition varies smoothly and uniformly during the cutting process.



(a) Cutting path generation for inner surface



(b) Cutting tool shape

Figure 5: Cutting path generation for inner surface and cutting tool shape

2.4 Determination of recommended cutting conditions

When polyurethane foam of support block is cutting along the cutter path generated in sculptured surface, poor form accuracy is easy to appear unless appropriate cutting conditions are applied because there is a large amount of deformation of the workpiece due to the elastic cushion. The determination of appropriate cutting conditions is a complex problem in that many factors such as feed speed and spindle speed, as well as machining direction, tool axial cutting depth, and spacing between paths, that must be simultaneously considered.

For this purpose, it tried to search the recommended cutting conditions by considering the characteristics that have a major influence on the form accuracy, that is based on the cutting conditions that have been accumulated empirically through the expert group. To solve this problem, the Taguchi technique [8, 9], which can easily evaluate the influence of each factor, was applied.

When the Taguchi technique is used, the influence of each factor of cutting conditions can be expressed in the form of a weight defined by the S/N ratio. This technique attempts to find the optimum levels for the controllable variables or design parameters. It applies a simple analysis of means to model the results, which gives quantitative information on the control factor effects. The smaller the error value of the form accuracy, the higher the machining quality expressed and the smaller the better characteristics.

So, it would possible to find out which condition is superior through the S/N ratio response table obtained by substituting the results of multiple experiments (N times) with form accuracy as a constraint as a local factor. In the S/N ratio response table, a small value corresponds to the best factor level, so if a cutting condition corresponding to a small value is found in the response table, this becomes the optimal condition in the corresponding environmental experiment area.

Here, the form accuracy is expressed by defining the distance difference between the original 3D model data and the 3D model target data of the finished workpiece. The 3D data of the finished workpiece were collected using commercial T-Scanner [10], and the comparison of surface data between the original and finished one was performed using the 3D shape analysis program named Geomagic Control X [11]. The average of the distance difference between the surfaces was converted in this program.

III. DETERMINATION OF OPTIMAL MANUFACTURING PARAMETERS

3.1 Experiment setup for searching optimal conditions

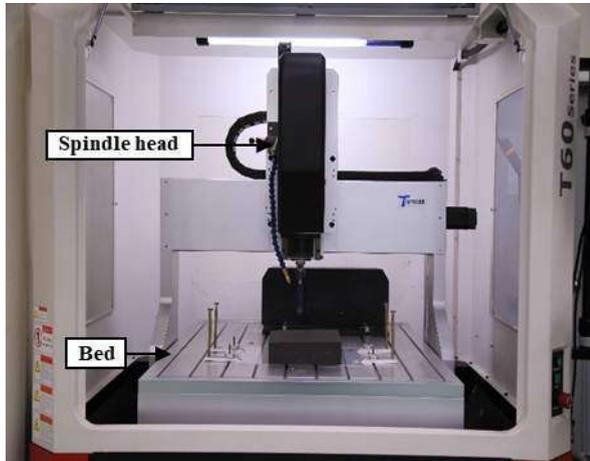
The initial cutting conditions to search for the optimal cutting conditions are to select the factor that has the greatest influence on the form accuracy, and apply experimentally for two factors: the tool path pattern in the inclined direction and the step over. The Tinyrobo's TinyCNC-6060 milling machine were used in this experiment, as shown in Figure 6, and a ball end mill for foam material manufactured by Taesan Solutions Co., Ltd. in Table 2 standard specification were used.

Table 2: Size specification of ball end mill used

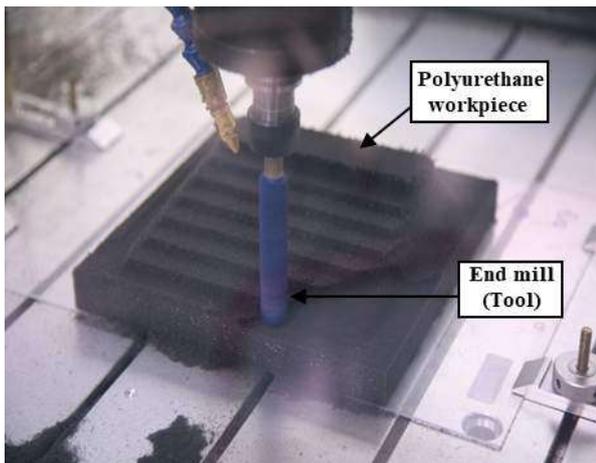
Shank diameter D1	10 mm	Body diameter D2	15 mm
Blade Diameter D3	16 mm	Blade accuracy	50 μ m
Blade length	80 mm	Sank length	50 mm
Particle height	0.5 mm	Particle width	1.4 mm
Size parameter	*Refer to Figure 5(b)		

The manufacturing model, as shown in Figure 7, was performed on three parts of the inclined model: a gentle slope(inclination angle of 12°), a sudden slope(inclination angle of 60°), and a corner. The initial cutting conditions were three conditions as shown in Table 3, which are already empirically applied in actual on-site machining. And, as a means to examine the stability of the cutting state, it confirmed the surface roughness measurement using the Mitsutoyo SJ-400

instrument by selecting the same location for each of the gentle slope (inclination angle 12°), sudden slope (inclination angle 60°), and corner. Also, this measurement applied to 9 samples that have been machined and set the cutoff value to 8 mm.



(a) NC milling machine



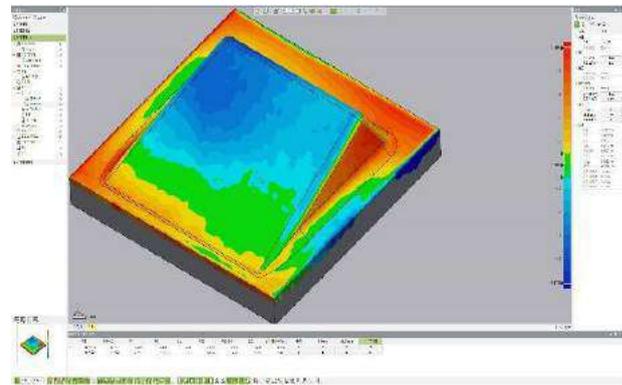
(b) Cutting process of polyurethane workpies

Figure 6: Configuration of NC milling machine and cutting process



(a) Perspective view

(b) Side view



(c) Analysis of form accuracy

Figure 7: Surface model used for inclined machining

On the other hand, the measurement of 3D shape accuracy takes into account the concentricity evaluation of the finished product. As shown in Figure 8, two shapes, spherical and cylindrical, were selected as target models. The three machining conditions were set in Table 3 in consideration of the steep slope in the spherical shape, and then the change value of the form accuracy according to the machining pattern was calculated as the S/N ratio by the Taguchi technique.

The definition of S/N ratio is different according to an objective function, that is, the characteristic value [13]. There are three kinds of characteristic value : Normal is Best (NB), Lower is Better (LB) and Higher is Better (HB). Equation (1) shows the formula for calculating the S/N ratio for the LB characteristic. LB is preferred to determine the best control factor level in the S/N ratio response table.

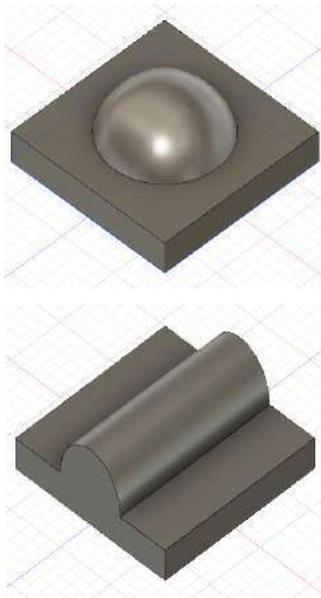
The S/N ratio of LB can be calculated by

$$S/N = -10 \log \left[\frac{1}{n} \sum_{i=0}^n y_i^2 \right] \quad (1)$$

where n is the number of measurements, and y_i the measured characteristic value.

Meanwhile, in the case of the spherical shape model, two types of machining are applied: a linear reciprocating pattern through raster machining, and a pattern machining the spherical surface with the ball end mill descending along the spiral slope through spiral machining. For

these models, both shape precision and concentricity were measured and compared.



(a) Spherical surface model
(b) Cylindrical surface model

Figure 8: Two kinds of 3D model used for machining verification

Table 3: Three kinds of initial machining condition setting

Conditions factor	unit	Comparison conditions		
		I	II	III
Spindle speed	rpm	1,800	2,000	2,200
Feedrate	mm/min	1,000	1,250	1,500
Step over	mm	0.5	0.6	0.7
pattern	direction	X-axis	Y-axis	Diagonal

Table 4 shows the results of form accuracy measured for each experimental condition and Table 5 is the evaluated result of Taguchi characteristic coefficient (S/N value) obtained by applying the cutting conditions of Table 3 to the form accuracy distribution of Table 4. According to these results, the S/N ratio shows a large difference of up to 280%.

For the object to be machined in Figure 7, the trends of the S/N ratio obtained through Equation (1) are shown in Figure 9 to Figure 11.

As a result, from the point of view of form accuracy, the average value at experiment No. 9 was good at the gentle slope, the value of No. 3

was more good at the sudden slope, and the value of No. 4 was best at the corner.

Table 4: Results of form accuracy for each condition (absolute value, mm)

Sample number	gentle slope	sudden slope	corner
1	0.2645	0.0895	0.2989
2	0.1175	0.0660	0.2770
3	0.1002	0.0148	0.3047
4	0.0660	0.0390	0.1175
5	0.1651	0.1475	0.3039
6	0.0670	0.0347	0.2390
7	0.2074	0.1779	0.4977
8	0.2426	0.6510	0.4725
9	0.0420	0.1315	0.9999

Table 5: Evaluated result of Daguchi Coefficient (Calculated S/N ratio)

S/N Ratio	Spindle speed (Lv. 1/2/3)			Feedrate (Lv. 1/2/3)		
	Step Over (Lv. 1/2/3)			Pattern (Lv. 1/2/3)		
Gentle Slope	15.0	19.2	14.7	14.1	14.8	22.7
	13.5	21.8	15.7	14.8	16.9	16.1
Sudden slope	23.8	22.1	8.0	18.6	8.2	22.0
	8.4	21.1	17.5	18.0	19.1	8.5
Corner	10.6	12.6	3.1	9.3	8.8	4.1
	9.1	4.4	8.4	4.4	9.0	9.6

3.2 Estimated result of optimal cutting conditions

When examining the optimal cutting conditions based on the case where the mesh characteristic value is small in the results of Table 5, first, for the case of the gentle slope machining, the spindle speed which is the condition III (2,200 rpm) in Table 3, is suitable. It can be seen that condition I (0.5mm) is most suitable for the amount of stepover, condition I (1,000mm/min) for the feed speed, and condition I (X-axis direction) for the pattern.

On the other hand, looking at the relative influence of each machining condition here, in the case of spindle speed and pattern, there is not much difference between each condition, but the difference between the maximum and minimum values in the feed rate and stepover is large.

In the case of sudden inclined part machining, the difference between the maximum and minimum values appears large in most cases. Condition III (2,200rpm) is suitable for spindle speed, but condition I (0.5mm) is the most suitable for the amount of stepover, and feed speed. Therefore, when viewed as a whole, the condition II (1,250mm/min) and the condition III (diagonal direction) are appropriate conditions.

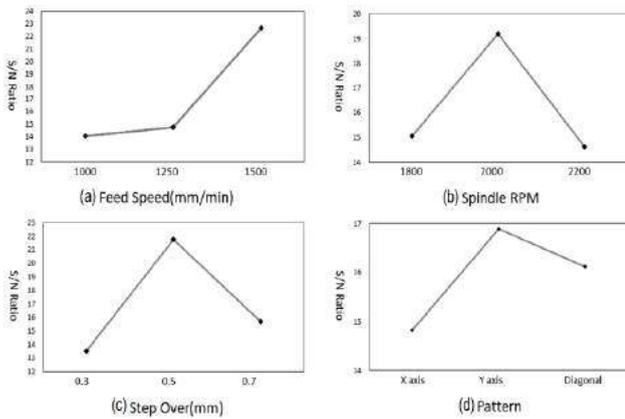


Figure 9: Main effects S/N ratio of a gentle slope

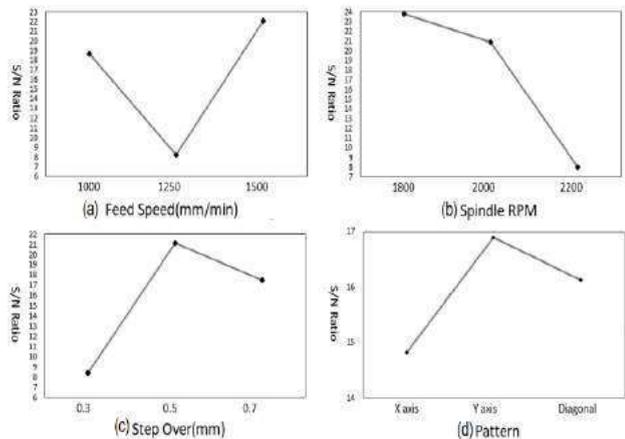


Figure 10: Main effects S/N ratio of a sudden slope

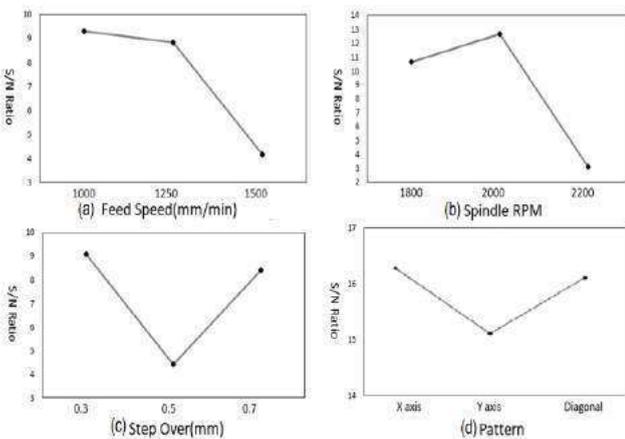


Figure 11: Main effects S/N ratio of a corner

In addition, the difference between the maximum and minimum values is generally large in the case of corner machining. Condition III (2,200 rpm) is suitable for the spindle speed, but condition II (0.6mm) is the most suitable for the stepover. Also, it can be seen that condition III (1,500 mm/min) for the feed speed and condition I (X-axis direction) for the pattern are appropriate.

In view of these results, when cutting regardless of the type of sculptured surface, that is considered as a case of cutting a sculptured surface including all shape elements such as a gentle slope, a sudden slope, and a corner, it is recommended to set the cutting conditions by considering the overall distribution of S/N values.

Table 6: The resulted optimal cutting condition

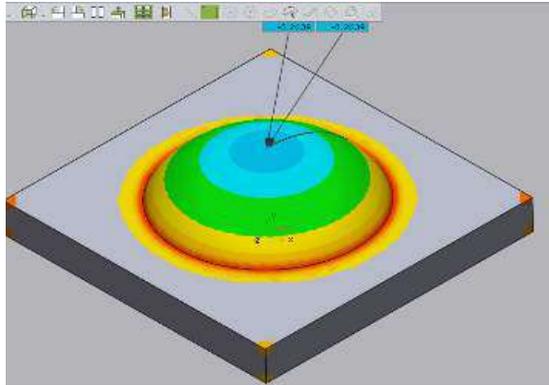
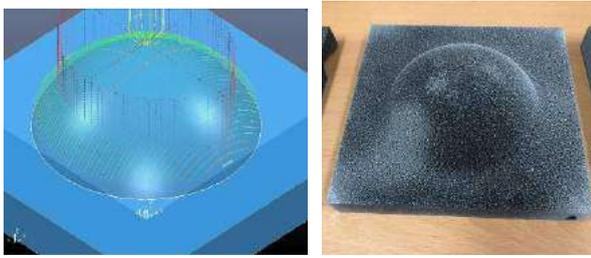
	gentle slope	sharp slope	corner
Spindle(RPM)	2000	1800	2000
Feed speed (mm/min)	1500	1250	1000
Step over(mm)	0.5	0.5	0.3
Pattern	Y axis	Y axis	Diagonal

Hence, in the environmental conditions targeted in this experiment, the spindle speed is set to No. III (2,200 rpm), the feed speed is set to No. II (1,250 mm/min), and the step-over is set to No. I (0.5 mm). And it can be determined that the pattern III condition (diagonal direction) is an appropriate condition.

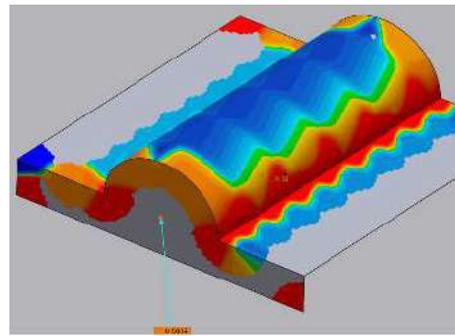
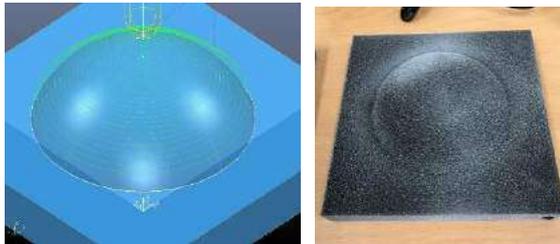
3.3 Measurement results of form accuracy

In order to verify the cutting characteristics of the cutting pattern according to the shape of the workpiece against the previously recommended cutting conditions, the form accuracy was examined for two models having spherical and cylindrical surfaces as shown in Figure 8.

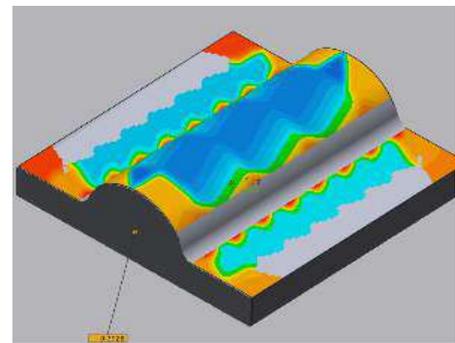
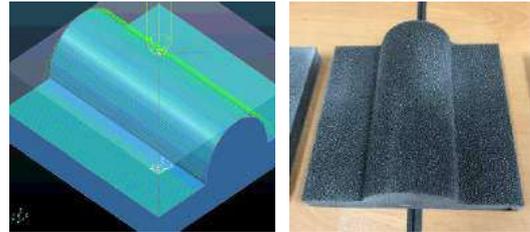
For the cylindrical surface model, the X-direction cutting pattern and the Y-direction cutting pattern were applied, and for the spherical model, the cutting patterns in the linear cutting direction and the spiral-linear direction were applied. At this time, the form accuracy of the machined product was measured with a 3D scanner and compared with the CAD prototype model of Figure 8.



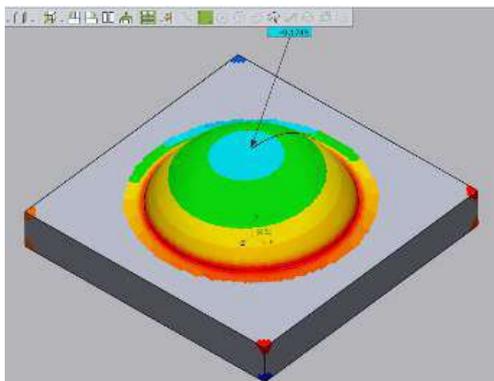
(a) Form accuracy for straight path



(a) Form accuracy for X-direction path



(b) Form accuracy for Y-direction path



(b) Form accuracy for spiral path

Figure 12: Form accuracy for straight and spiral path applied to spherical model

Figure 13: Form accuracy for X and Y-direction path applied to cylindrical model

Table 7: Comparison of concentricity error for each model

Spherical	Concentricity Error (mm)	Cylindrical Model	Concentricity error (mm)
Straight direction	0.2639	X axis direction	0.5039
Spiral direction	0.1749	Y axis direction	0.3925

The error distribution diagram is shown in Figure 12 to Figure 13, in the form of a distribution map according to the chromaticity applied to the surface.

As a result, it can be seen that the shape error (the amount of deformation of the workpiece) is largely generated in a portion or a corner portion having a sudden inclination. Also, by inputting these scanned data into the Geomagic Control X

program [11, 12], the center coordinate eccentricity of the regression analysis surface between the original CAD model and the measured cloud data was obtained, and this was calculated as the concentricity of the spherical surface and the cylinder. The results are shown in Table 7.

Here, the concentricity can be viewed as a scattering of the shape accuracy error for the processed sculptured surface. When evaluating the form accuracy according to the cutting pattern, the error is the largest at 0.5039 mm when the cylindrical surface is processed in the X direction.

When the spherical surface was processed in the vortex-linear direction, it was found to be the smallest as 0.1749 mm, indicating that the shape accuracy when machining the spherical surface in the vortex-linear direction was the best.

In addition, when comparing only the machining of the spherical and cylindrical surfaces regardless of the cutting pattern, it shows that the form accuracy when machining the spherical surface is superior to that of machining the cylindrical surface, which is the slope of the cutting path or the amount of step-over due to the nature of the workpiece. It can be said that the smaller the change in, the better the form accuracy is.

3.4 Review of packaging performance by vibration test

In order to examine the packaging performance according to the clearance of the packaging surface, an experiment was conducted on packaged products and boxes. This experiment was conducted for four packaging methods: PU(polyurethane) packaging with small gap which is machined by recommended machining conditions in this study, PU foam packaging with large gap which is machined by conventional cutting conditions, cotton felt packaging using a goft cotten fiber cloth, and bubble wrap packaging using vinyl with bubble for general shock mitigation.

The process of machining of support block and packaging for this experiment is as shown in Figures 14 (a) to (d). Figure 14(a) is the process of

cutting the PU material on the NC milling machine, and Figure 14(b) is the process of inserting the content goods into the support block. The Figure 14(c) is the process of putting the support block into the packaging box, and Figure 14(d) shows the process of mounting it on the vibrator for the vibration test.

The vibration test standards related to the frequency band affecting the packaging should follow the vibration test method of KS A ISO 1017. The frequency was linearly increased from 10 Hz to 40 Hz for 15 minutes.



(a) Machine the sculpture surface on the PU support block



(b) Placement of the contents on the support block



(c) Inserting inside the box



(d) Mount the packaging box on the vibration tester

Figure 14: Arrangement for the vibration shock experiment

In order to know the vibration displacement input from the excitation tester according to each packaging method, an accelerometer is attached to the side of the packaging box to achieve 10Hz and 20Hz. The input amplitude was measured at 30 Hz and 40 Hz and compared with the amplitude of the package contents.

In this vibration test, vibration is given under the same conditions for each packaging method, and the RMS (root mean square) acceleration value as for each 1 Hz section is obtained through the response acceleration according to the time as shown in Equation (2), and the vibration level $dB(V)$ is calculated using Equation (3).

$$a_{rms} = \sqrt{\frac{1}{T} \int_{t_i}^{t_{i+1}} (t)^2 dt} \quad (2)$$

$$dB(V) = 20 \log \log \frac{a_{rms}}{10^{-6}} \quad (3)$$

Where a is the acceleration response, T is time taken to increase by 1 Hz, and $T = t_{i+1} - t_i$.

The estimated RMS acceleration value and vibration level was compared for each method. At this time, the acceleration sensor was attached so that the X-axis direction was the direction of gravity.

Table 8 is the data comparing the amplitude of the input from the vibration tester for each frequency and the amplitude of the package contents. In Figure 15, the ratio of the amplitude of the packaged contents to the amplitude input from the vibration tester is compared and graphed for comparison. The smaller the value, the greater the decrease in the input amplitude.

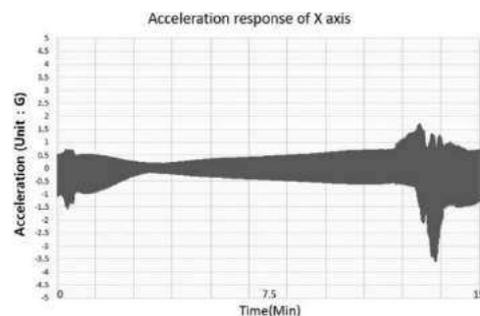
Table 8: Amplitude of frequency interval by packaging method (Unit : mm)

		10 Hz	20 Hz	30 Hz	40 Hz
PU package with small gap	content	1.171	0.179	0.171	0.196
	box	1.348	1.134	1.141	1.205
PU package with large gap	content	2.102	1.287	0.63	0.678
	box	1.348	1.134	1.142	1.205
Cotton felt	content	0.975	1.275	2.125	1.697
	box	1.355	1.142	1.149	1.207
Bubble wrap	content	2.359	1.232	0.678	0.272
	box	1.131	1.135	1.147	1.206

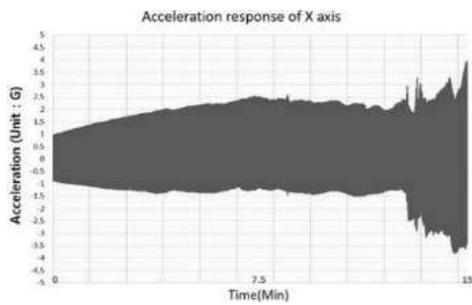
The PU packaging support block with small gap, which is machined by recommended manufacturing conditions of this study, shows very stable support performance in all frequency ranges compared to other packaging methods.

Figure 15 shows the acceleration response according to each packaging method, and Figure 16 shows the vibration level for each packaging method in a table for comparison.

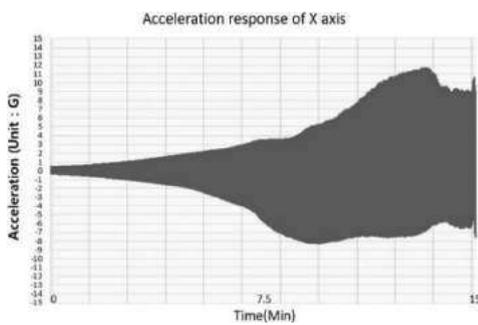
In the case of PU packaging with large gap and the cotton felt packaging, it was confirmed that the packaged product was not properly supported over the entire frequency range and showed a large range of vibration levels.



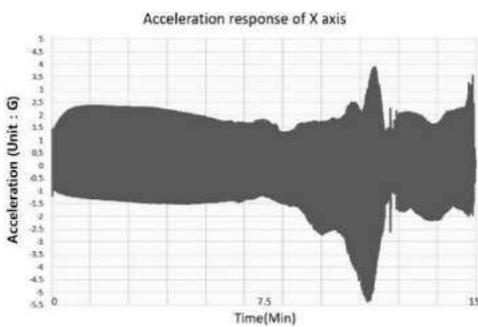
(a) PU packing with small gap



(b) PU packing with large gap



(c) Cotton felt



(d) Bubble wrap

Figure 15: Acceleration response of each packing method

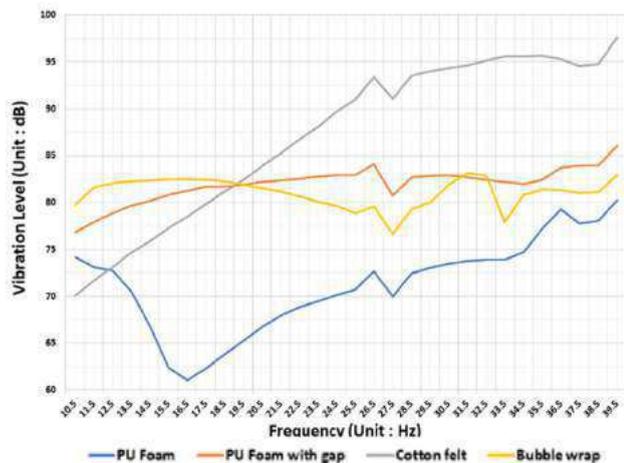


Figure 16: Vibration level of each packing supports method

In the case of packaging using bubble wrap, it has a large amplitude range in the range of 10 Hz to 20 Hz. Also, the vibration is stabilized thereafter, so it can be confirmed that the vibration level temporarily rises around the 30 Hz section.

Therefore, it was found that the PU pavement with small gap showed a better amplitude reduction rate than other packaging methods after 20Hz.

IV. CONCLUSION

Because the polyurethane materials used for packaging support block of valuables have high cushion and elasticity, it is not easy to manufacture them while maintaining form accuracy, which is an important factor that allows the contents to be well protected from shock or vibration during the transfer process. For this reason, it is also very important to well determine various manufacturing parameters in the machining of packaging support block.

This study explored the manufacturing conditions that can maintain the form accuracy of the contact surface so that the support block can stably support the contents. As these parameters, not only feed speed and spindle speed, but also many factors such as machining direction, tool axial cutting depth, and spacing between paths, are considered in a complex manner.

Based on the manufacturing data accumulated by a group of field experts for a long time, the search process of the optimal condition using the Taguchi's method was applied. The optimal conditions were searched through these analysis results, considering the characteristics value that affect the form accuracy as the initial conditions, and considering the mesh characteristic values of the Taguchi technique derived from main effect S/N ratio for a gentle slope, sudden slope, and a corner.

As a result, it was found to be optimal that the appropriate feed rate is 1,250 mm/min, the spindle speed is 2,200 rpm, and the stepover is 0.5 mm in the case of cutting a sculptured surface that includes all of a gentle slope, a sudden slope, and a corner. Also, it could be revealed that it is excellent to select the diagonal direction for the

cutting patterns, and the PU packing with small gap, which is machined by recommended manufacturing conditions of this study, showed very stable support performance in all frequency ranges compared to other packaging methods in the experiment of vibrational shock test.

However, since these optimal conditions were limited to the environment and to the machinability of the ball end mill used in this study, these conditions may change a lot if the machinability of these tools is different. For this case, if this algorithm is supplemented with the wide range of experience data when a ball end mill of a different shape is applied, it could be used as it is expected that the conditions in the corresponding environment can be expanded to general manufacturing purpose.

For the follow-up study, it is suggested that a lot of empirical data on a wider range of conditions and environments should be accumulated and applied. If a lot of comprehensive cutting data is accumulated for various support block materials with different hardness and elastic modulus, it is thought that it will be possible to derive optimized conditions in the applicable environment by applying the methodology in this study. In addition to the Taguchi method in which such a large amount of data is secured, it is considered possible to use big data-based self-learning artificial intelligence techniques.

ACKNOWLEDGEMENTS

This research was conducted with the support of research funding for general projects in the Seoul National University of Science and Technology.

REFERENCES

- Hyun Mo, J., Su Il, Kim., (2015), Random Vibration Characteristics of Fruits in Packaging System for Parcel Delivery Service, Korean journal of packaging science & technology, 21(2), 67-71.
- J. G. Kim, J. Y. Kim, H. S. Kim, (2019), Design for Improving Impact Resistance of Microwave Oven Using Drop-Impact Analysis, Journal of the Korean society for power system engineering, 13(3), 53-58.
- Nam-Hun, Kim., (2012), Selection of the Optimal Machining Condition for a High-hardness Resin using the 5-axis Machine, Journal of the Korean Society of Manufacturing Process Engineers, 11(5), 29-34.
- Se-Hong, Min., Hui-Song, Kim., (2000), A Study of an Effect of Tool Offset on Cutting Precision Considering Cutting Force in Polyurethane Foam Cutting, The Korean Society of Mechanical Engineers, 24(12), 3018-3025. <https://doi.org/10.22634/KSME-A.2000.24.12.3018>.
- Zhang, Y., and Wu, Z., (2007), Offset Face Gear Drives: Tooth Geometry and Contact Analysis, Journal of Mechanical Design, 119(1), 114-119. <https://doi.org/10.1115/1.2828772>.
- Shim, V, P, W., Tu, Z, H., Lim, C, T., (2000), Two-dimensional response of crushable polyurethane foam to low velocity impact, International Journal of Impact Engineering, 24(6), 703-731. [https://doi.org/10.1016/S0734-743X\(99\)00149-9](https://doi.org/10.1016/S0734-743X(99)00149-9).
- Hyung-Seok, Kim., Boo-Yoon, Lee., and Sanghoon, Lee., (2018), Drop Impact Analysis of Outside Cooling Unit Package of System Air-Conditioner and Experimental Verification, Journal of the Korea Academia-industrial Cooperation Society, 19(4), 111-116. <https://doi.org/10.5762/KAIS.2018.19.4.111>
- Tae Ha, K., Chang Hee, S., Rac Gyu, L., (2013), Optimization of Design Parameters for Lock-Claws of Pneumatic Fitting Using Taguchi Method, Transactions of the Korean Society of Mechanical Engineers, 37(12), 1541-1546. <https://doi.org/10.3795/KSME-A.2013.37.12.1541>.
- Jun Wei, L., Jian, J., Tae Jo, K., and Dae Kyun, B., (2013), Study of Optimal Machining Conditions of Ultrasonic Machining By Taguchi's Method, Transactions of the Korean Society of Mechanical Engineers - A, 37(2), 213-218. <https://doi.org/10.3795/KSME-A.2013.37.2.213>.
- T-Scan Manual, TaeSan Solution Ltd., (2016), 1-75.
- Hee young, M., (2014), Development of automation devices for the 3D digital

measuring and preservation of archival artifacts, Annual Research Report, National Archives, Ministry of Security and Public administration, 1-286. <https://doi.org/10.23000/TRKO201500011134>.

12. Suin, E., (2019), A Study on the Machining Condition of 3D Shape Polyurethane Packaging Support, Master's thesis, Seoul National Univ. of Science & Technology.
13. William, Y, Fowlkes., & Clyde, M, Creveling., (1995), Engineering Methods for Robust Product Design : Using Taguchi Methods in Technology and Product Development, Addison Wesley Publishing Company, Reading, Massachusetts, 54-59.
14. Suin, E., Jiwan, K., and Heeyoung, M., (2021), A Study on the Optimum Machining Conditions of Polyurethane Materials used for Valuable Packaging Blocks, International Journal of u - and e - Service, Science and Technology, 14(2).